

Nonequilibrium mode-coupling theory for driven granular systems

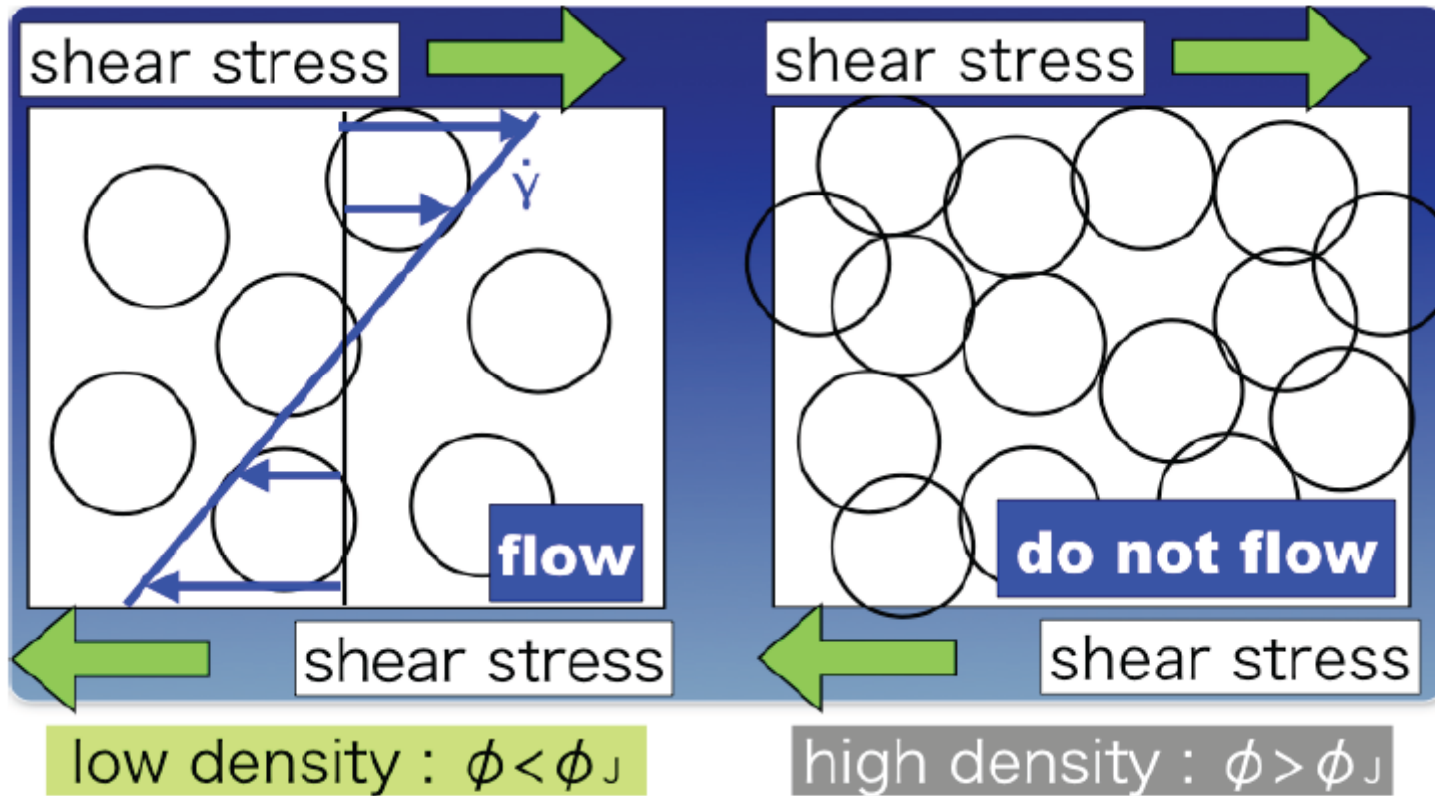
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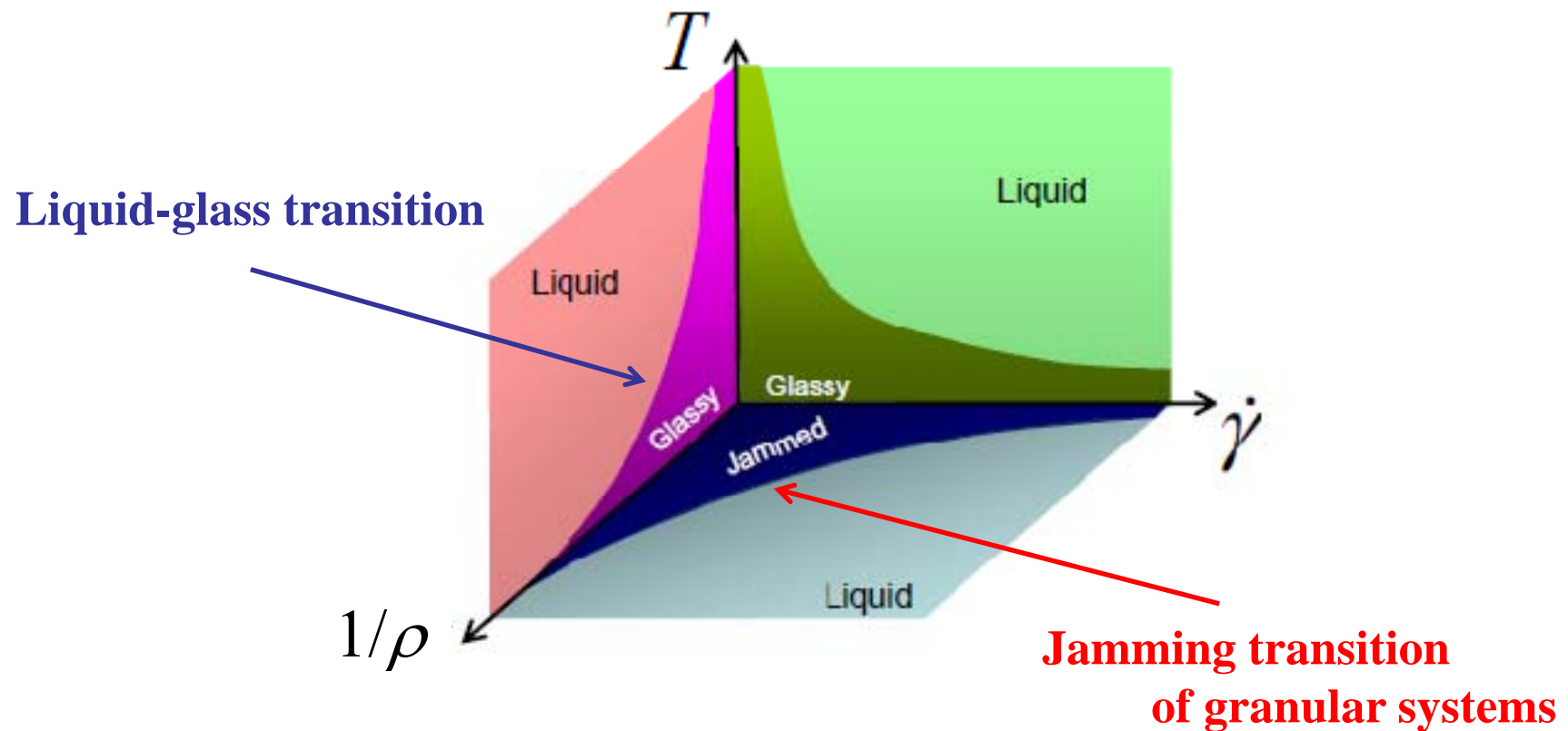
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Jamming transition of granular systems



ϕ : density, ϕ_J : critical density

Motivation : unified understanding of jamming phase diagram



Liu and Nagel, Nature 396, 21 (1998)

Characteristic features of granular systems

- **Dissipative system (inelastic collisions)**
 - **coupled with heat bath of $T = 0$**
- **External load necessary to make it fluidized**
 - **e.g., shearing, shaking**
- **Intrinsic nonequilibrium system**
 - **linear response theory not applicable**
 - **no detailed balance**
 - time-reversal symmetry broken**
 - Langevin equation not applicable**



Liquid theory for linear transport coefficients

- Green-Kubo relation

$$D = \int_0^{\infty} dt \langle v_z(t) v_z(0) \rangle, \quad \eta = \frac{1}{k_B T V} \int_0^{\infty} dt \langle \sigma_{xy}(t) \sigma_{xy}(0) \rangle$$

- Generalized Langevin equation (Mori-Zwanzig equation)

$$\frac{\partial}{\partial t} Z(t) + \int_0^t ds M(t-s) Z(s) = 0 \quad \text{for } Z(t) = \langle v_z(t) v_z(0) \rangle$$

- Approximate theory for memory kernel (e.g. mode-coupling theory)

$$M(t) = \frac{\rho k_B T}{6\pi^2 m} \int dk k^4 c(k)^2 F_s(k, t) F(k, t)$$

steady-state properties arbitrarily far from equilibrium?

Nonequilibrium mode-coupling theory (MCT) for sheared granular systems

1. Generalized Green-Kubo relation

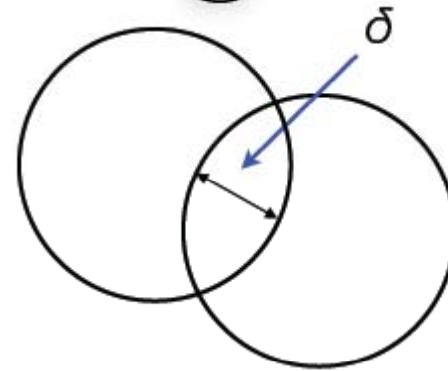
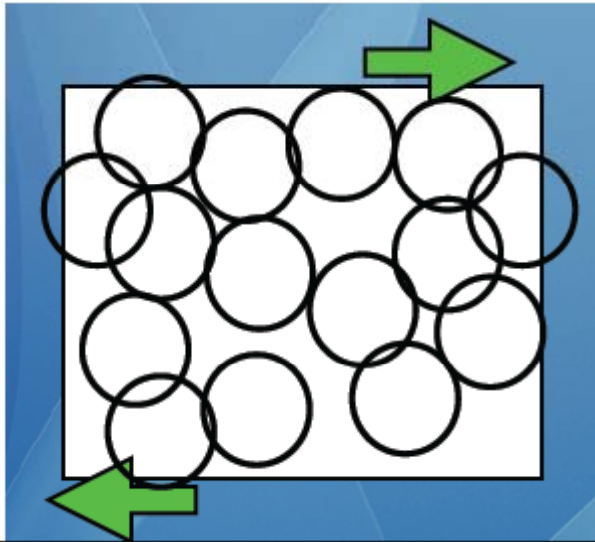
for nonequilibrium steady-state properties
in terms of **transient time-correlation function**

2. Mori-Zwanzig equation of motion

for transient time-correlation function

3. Mode-coupling approximation

Model (frictionless grains)



$\Delta=1$ (Linear model)

$\Delta=3/2$ (Hertz model)

Interaction Force : $F=k\delta^\Delta$

Compressed Length : δ

The exponent for the interaction : Δ

Dissipative force between the contacting particles

SLLOD equations of motion

- **SLLOD equations of motion**

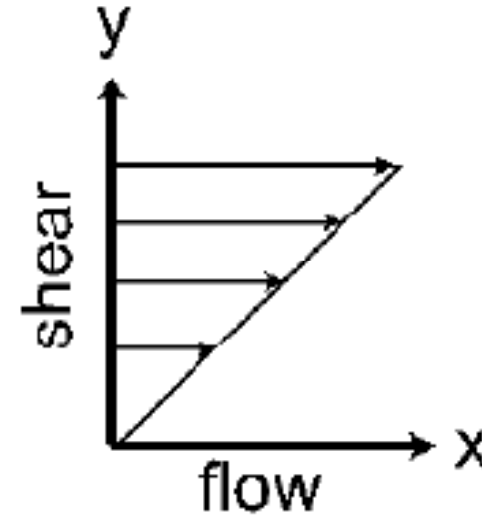
$$\dot{\mathbf{r}}_i = \mathbf{p}_i/m + \boldsymbol{\kappa} \cdot \mathbf{r}_i$$

$$\dot{\mathbf{p}}_i = \sum_{j \neq i} (\mathbf{F}_{ij}^{\text{el}} + \mathbf{F}_{ij}^{\text{vis}}) - \boldsymbol{\kappa} \cdot \mathbf{p}_i$$

$\dot{\mathbf{r}}_i$: velocity

\mathbf{p}_i : peculiar momentum with respect to $\mathbf{u}(\mathbf{r}_i) = \boldsymbol{\kappa} \cdot \mathbf{r}_i$

$\boldsymbol{\kappa}$: shear rate tensor



$$\kappa_{\lambda\mu} = \dot{\gamma} \delta_{\lambda x} \delta_{\mu y}$$

$\mathbf{F}_{ij}^{\text{el}} = \hat{\mathbf{r}}_{ij} \Theta(d - r_{ij}) f(d - r_{ij})$: conservative force (e.g. $f \sim x$, $f \sim x^{3/2}$)

$\mathbf{F}_{ij}^{\text{vis}} = -\hat{\mathbf{r}}_{ij} \Theta(d - r_{ij}) \zeta(d - r_{ij}) (\mathbf{g}_{ij} \cdot \hat{\mathbf{r}}_{ij})$: dissipative force (e.g. $\zeta = \text{const}$, $\gamma \sim x^{1/2}$)

with $\mathbf{r}_{ij} = \mathbf{r}_i - \mathbf{r}_j$ and $\mathbf{g}_{ij} = \dot{\mathbf{r}}_i - \dot{\mathbf{r}}_j$

Liouville equation

- Liouville equation for the phase-space variable $A(\Gamma)$ with $\Gamma = (r^N, p^N)$

$$\frac{d}{dt} A(\Gamma) = \dot{\Gamma} \cdot \frac{\partial}{\partial \Gamma} A(\Gamma) \equiv iL A(\Gamma)$$

formal solution : $A(\Gamma(t)) = \exp(iLt)(\Gamma(0))$

- Liouville equation for the phase-space distribution function $f(\Gamma, t)$

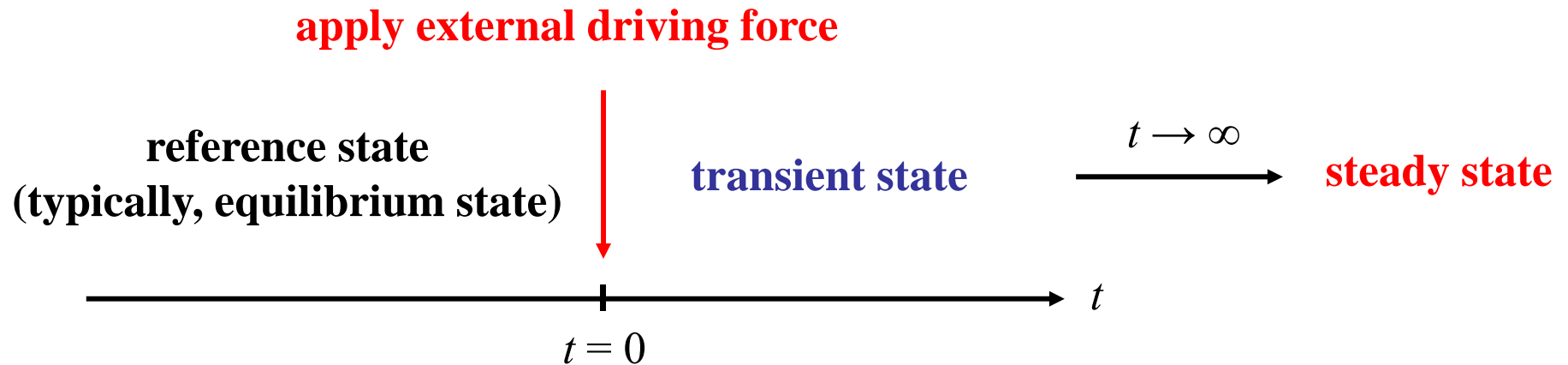
$$\frac{\partial}{\partial t} f(\Gamma, t) = - \left[\dot{\Gamma} \cdot \frac{\partial}{\partial \Gamma} + \left(\frac{\partial}{\partial \Gamma} \cdot \dot{\Gamma} \right) \right] f(\Gamma, t) \equiv -iL^* f(\Gamma, t)$$

$$iL^* = iL + \Lambda \quad \text{with} \quad \Lambda = \frac{\partial}{\partial \Gamma} \cdot \dot{\Gamma} = -\frac{1}{m} \sum_i \sum_{j \neq i} \Theta(d - r_{ij}) \zeta(d - r_{ij})$$

formal solution : $f(\Gamma, t) = \exp(-iL^* t) f(\Gamma, 0)$

Reference state for granular systems?

- Conventional method for handling external driving force



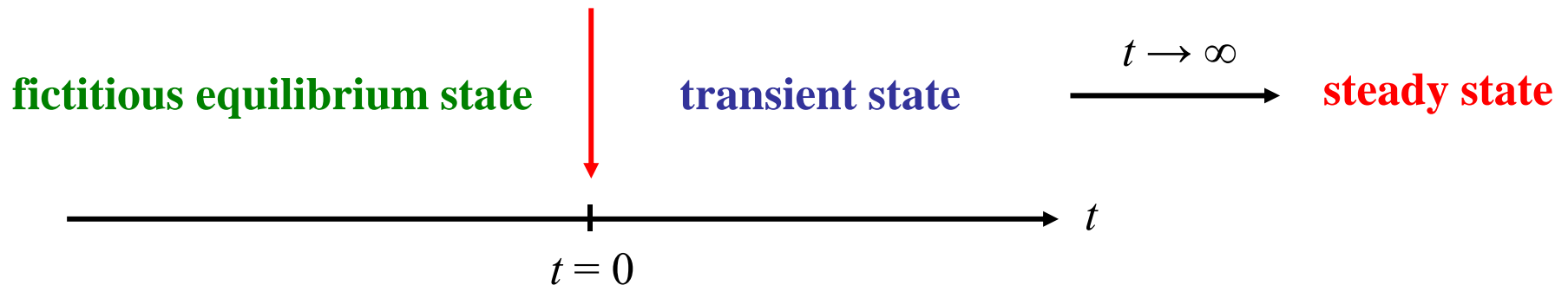
- Naïve quiescent equilibrium state does not exist for granular systems due to the presence of inelastic collisions !

Our recipe

reference state : fictitious equilibrium state

in which dissipative forces are turned off

apply external driving force
+ turn on dissipative forces



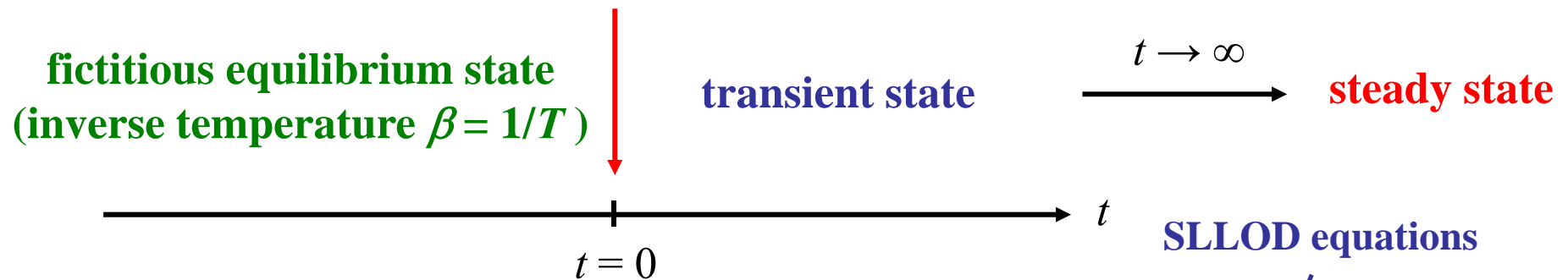
Does it make sense?

Yes !

**steady-state properties do not depend
on the choice of the reference state**

Implementation of our recipe

apply external driving force
+ turn on dissipative forces



➤ nonequilibrium phase-space distribution function : $f(\Gamma, t) = \exp(-iL^*t) f_{\text{eq}}(\Gamma; \beta)$

➤ nonequilibrium average : $\langle A(t) \rangle_{\beta} \equiv \int d\Gamma A(\Gamma) f(\Gamma, t)$

➤ steady-state average : $\langle A \rangle_{\text{ss}} \equiv \lim_{t \rightarrow \infty} \langle A(t) \rangle_{\beta}$

➤ identity : $e^{-iL^*t} = 1 + \int_0^t ds e^{-iL^*s} (-iL^*)$

Generalized Green-Kubo relation

(S.-H. Chong, M. Otsuki, and H. Hayakawa, Phys. Rev. E 81, 041130 (2010))

$$\langle A \rangle_{\text{ss}} = \langle A(0) \rangle_{\beta} + \int_0^{\infty} ds \langle A(s) \Omega(0) \rangle_{\beta}$$



transient time-correlation function

- Dissipation function**

$$\Omega = -\beta \dot{\gamma} \sigma_{xy} - 2\beta R - A$$

with

$$\left\{ \begin{array}{l} \sigma_{xy} = \sum_i \left[\frac{p_i^x p_i^y}{m} + x_i \sum_{j \neq i} (F_{ij}^{\text{el}, y} + F_{ij}^{\text{vis}, y}) \right] \\ R = \frac{1}{4} \sum_i \sum_{j \neq i} \Theta(d - r_{ij}) \zeta(d - r_{ij}) (\mathbf{g}_{ij} \cdot \hat{\mathbf{r}}_{ij})^2 \\ A = -\frac{1}{m} \sum_i \sum_{j \neq i} \Theta(d - r_{ij}) \gamma(d - r_{ij}) \end{array} \right.$$

- e.g. steady-state shear stress** : $\sigma_{xy}^{\text{ss}} \equiv -(1/V) \lim_{t \rightarrow \infty} \langle \sigma_{xy}(t) \rangle_{\beta}$

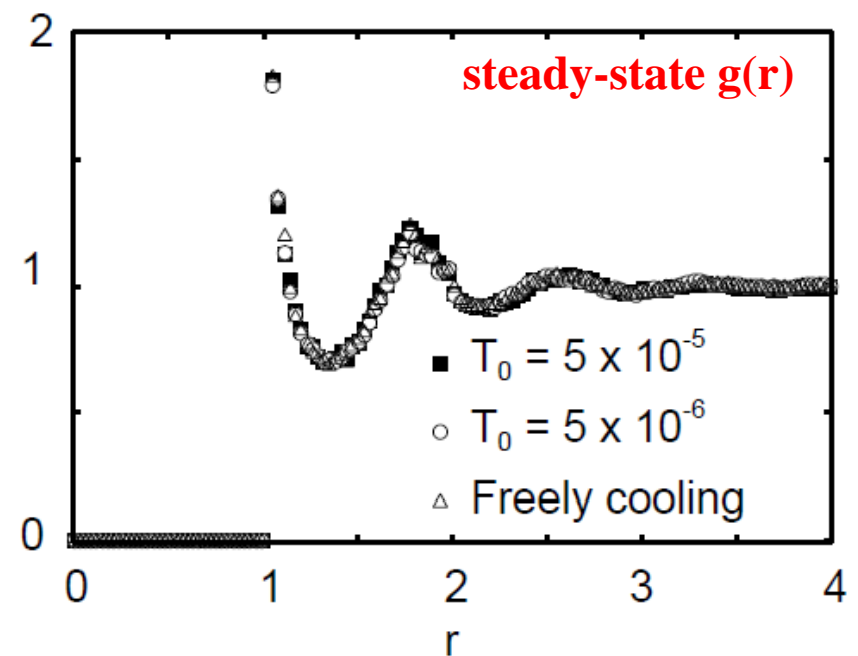
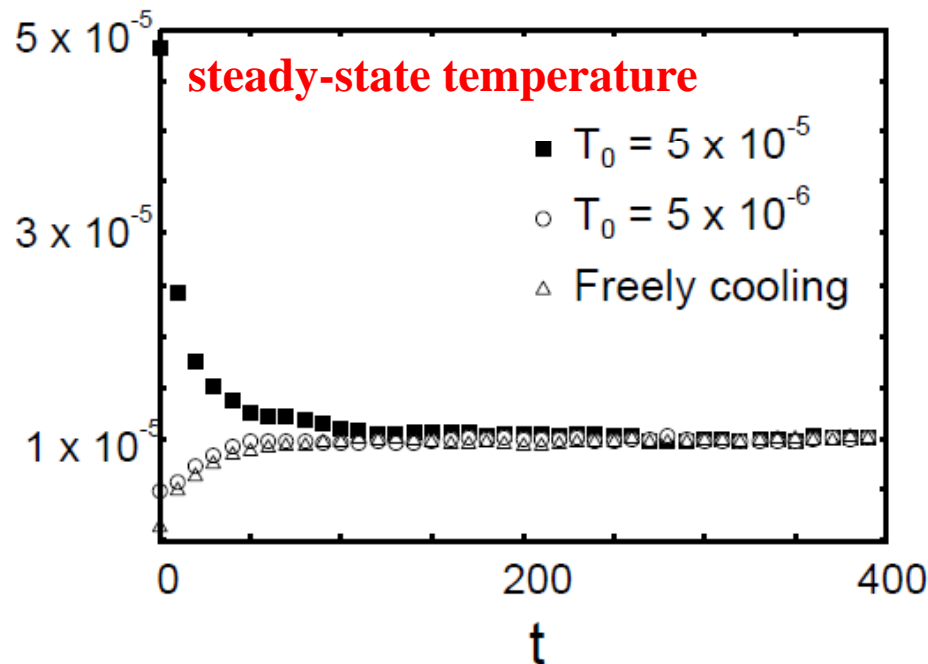
$$\sigma_{xy}^{\text{ss}} = \frac{\beta \dot{\gamma}}{V} \int_0^{\infty} ds \langle \sigma_{xy}(s) \sigma_{xy}(0) \rangle_{\beta} + \frac{2\beta}{V} \int_0^{\infty} ds \langle \sigma_{xy}(s) R(0) \rangle_{\beta} + \frac{1}{V} \int_0^{\infty} ds \langle \sigma_{xy}(s) A(0) \rangle_{\beta}$$

Justification of our recipe

- One can show that $\frac{\partial}{\partial \beta} \langle A(t) \rangle_{\beta} = \langle A(t) \rangle_{\beta} \langle H_0(0) \rangle_{\beta} - \langle A(t) H_0(0) \rangle_{\beta}$

- For systems that exhibit *mixing* $\left(\lim_{t \rightarrow \infty} \langle A(t) B(0) \rangle = \langle A(t) \rangle \langle B(0) \rangle \right)$

there holds $\lim_{t \rightarrow \infty} \frac{\partial}{\partial \beta} \langle A(t) \rangle_{\beta} = 0$, i.e., $\langle A \rangle_{ss} = \lim_{t \rightarrow \infty} \langle A(t) \rangle_{\beta}$ is independent of β .



Remarks for the rest of the steps

- **Anisotropic nature of the sheared system**

$$C_{\lambda\mu}(\mathbf{q}, t) \neq \hat{q}_\lambda \hat{q}_\mu C_L(q, t) + (\delta_{\lambda\mu} - \hat{q}_\lambda \hat{q}_\mu) C_T(q, t) \quad (\lambda, \mu = x, y, z)$$

- **Non-Hermitian nature of the Liouville operator**

$$\langle [iLA(t + \tau)] B(t)^* \rangle = -\langle A(t + \tau) [iLB(t)^*] \rangle + \langle A(t + \tau) B(t)^* \Omega(0) \rangle$$

- **Velocity-dependent dissipative force**

couplings to $\rho(k) j(p)$ as well as the ones to $\rho(k) \rho(p)$

must be taken into account in the mode-coupling approximation

MCT equations for transient density correlator

- **Zwanzig-Mori equation of motion**

$$A_q^{\lambda\mu} = \frac{\rho}{m} \int dr (1 - e^{iq \cdot r}) \hat{r}^\lambda \hat{r}^\mu \Theta(d-r) \gamma(d-r) g(r)$$

$$\left[\frac{\partial}{\partial t} - \underline{q \cdot \kappa \cdot \frac{\partial}{\partial q}} \right] F_q(t) = q \cdot H_q(t)$$

dissipative force

$$\left[\frac{\partial}{\partial t} - \underline{q \cdot \kappa \cdot \frac{\partial}{\partial q}} \right] H_q^\lambda(t) = - \left(q_\lambda \frac{v^2}{S_q} + B_q^\lambda \right) F_q(t) - A_q^{\lambda\mu} H_q^\mu(t) - \underline{[\kappa \cdot H_q(t)]_\lambda}$$

anisotropy due to shear

$$- \int_0^t ds \underline{M_q^{\lambda\mu}(s)} H_{q(s)}^\mu(t-s) - \int_0^t ds \underline{L_q^\lambda(s)} F_{q(s)}(t-s)$$

non-Hermitian nature of iL

- **MCT expression for the memory kernel**

$$M_q^{\lambda\mu}(t) = \frac{\rho}{2(2\pi)^3 v_T^2} \int d\mathbf{k} \left[V_{q,k,p}^{(\text{el})\lambda} - V_{q,k,p}^{(\text{vis})\lambda} \right] V_{q(t),k(t),p(t)}^{(\text{el})\mu} F_k(t) F_p(t)$$

$$+ \frac{1}{(2\pi)^3 v_T^2} \int d\mathbf{k} D_{q,k,p}^{\lambda\nu} V_{q(t),k(t),p(t)}^{(\text{el})\mu} F_k(t) H_p^\nu(t) + \dots$$

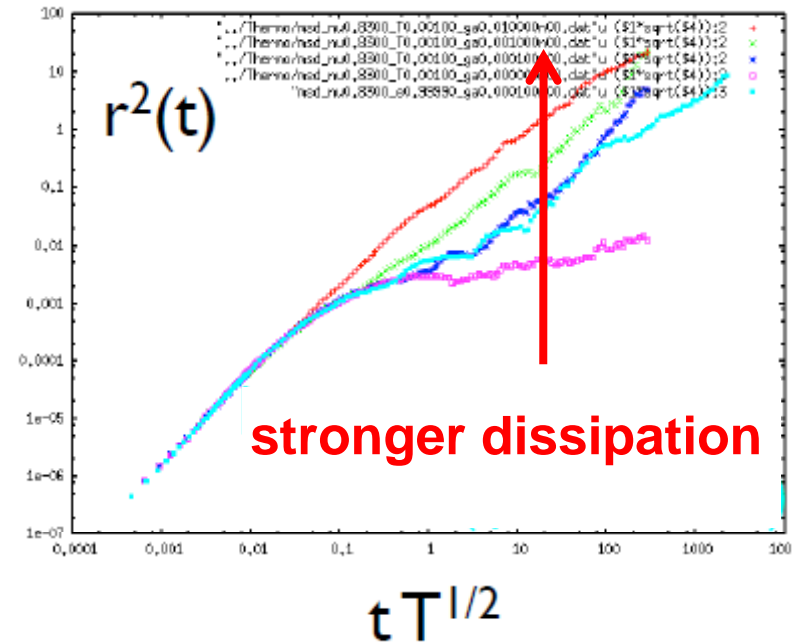
$$V_{q,k,p}^{(\text{el})\lambda} = v_T^2 (k_\lambda c_k + p_\lambda c_p), \quad V_{q,k,p}^{(\text{vis})\lambda} = (C_k^\lambda + C_p^\lambda) / \rho, \quad D_{q,k,p}^{\lambda\mu} = A_p^\lambda - A_k^\lambda$$

Implications of the theory

$$M_q^{\lambda\mu}(t) = \frac{\rho}{2(2\pi)^3 v_T^2} \int d\mathbf{k} \left[\underbrace{V_{q,k,p}^{(\text{el})\lambda}}_{\text{elastic force (cage effect)}} - \underbrace{V_{q,k,p}^{(\text{vis})\lambda}}_{\text{dissipative force}} \right] \underbrace{V_{q,k,p}^{(\text{el})\mu}}_{\text{elastic force (cage effect)}} F_k(t) F_p(t) + \dots$$

- **Vanishing of the plateau**
due to the dissipative force

- **Singular behavior near**
the jamming transition point



$$g(r) = A\delta(r-d) + \dots \rightarrow V_{q,k,p}^{(\text{el})\lambda} = O(1/k) \rightarrow \lim_{t \rightarrow \infty} F_q(t)/S_q = 1 \text{ for all } q$$

Summary

- **Nonequilibrium mode-coupling theory is developed for driven, dense granular systems.**
- **The theory is of the same quality as that for the glass transition.**
- **It is hoped that the theory is useful for a unified understanding of the glass transition and the jamming transition.**